



**TraFi**

Liikenteen turvallisuusvirasto

**SAE G-12 AWG  
Athens 2017**

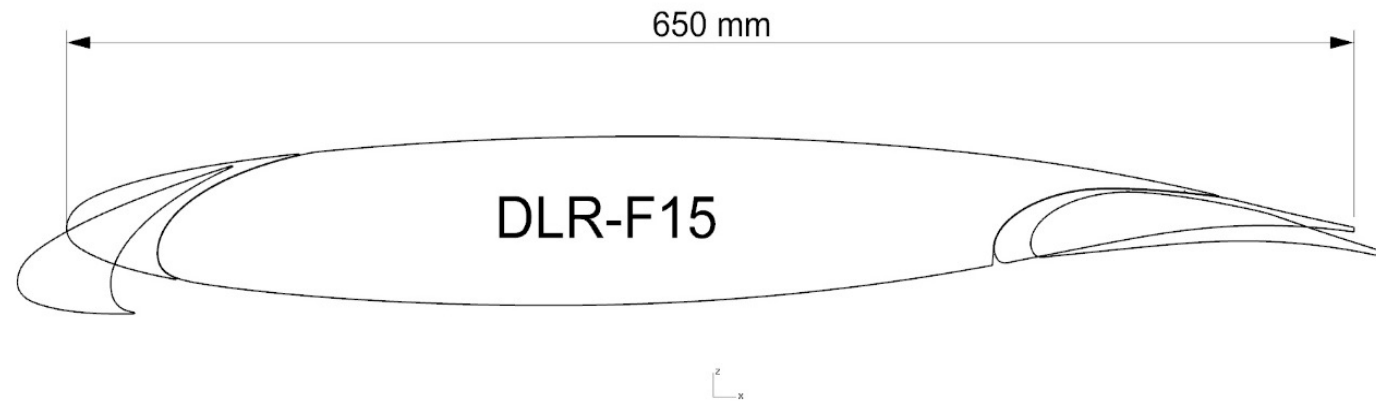
# *Frostwing Preliminary Results*

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Arteform Ltd*

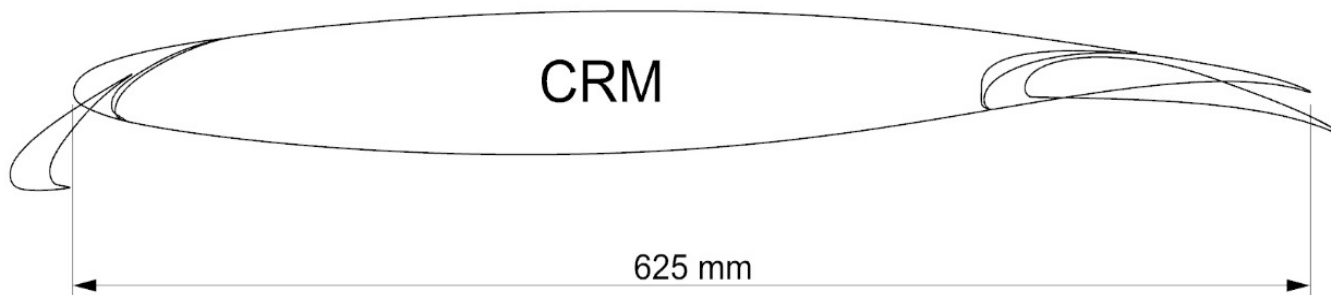
*Vastuullinen liikenne.  
Yhteinen asia.*

- ***2D Wing Section Model W/T Tests***
  - ***Fluid Tests***
  - ***CSFF Tests***
  
- ***CFD Studies and Flat Plate W/T Tests***
  - ***CFD Modeling of a Flat Plate with a Fluid layer***
  - ***Flat Plate Tests in Wind Tunnel***

# 2D Wing Section Models



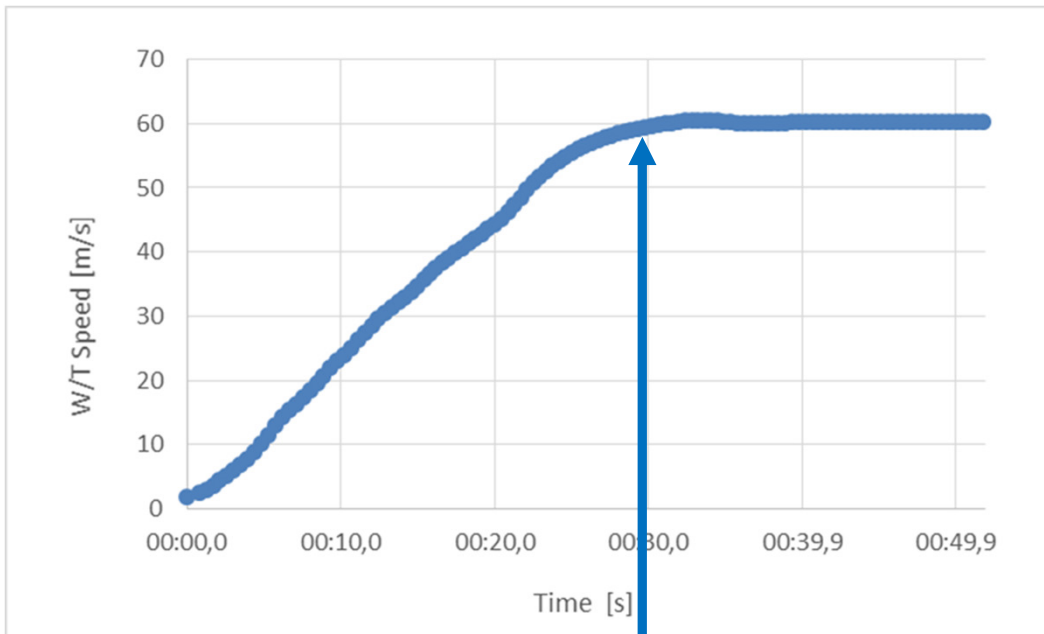
*DLR-F15  
W/T tests  
2012-2014.  
(IW-project)*



*HL-CRM Mod.  
W/T tests  
started 2016*

# W/T Measurement program

## W/T speed and AoA sequence



*Rotation*

Wing section	Slat/Flap angle	Ground Roll $\alpha$	Ground Roll $C_1$	$\alpha$ at $V_2$	$C_1$ at $V_2$
DLR – F15	S11° /F5°	0°	0.51	8.0°	1.28
CRM	S22°/F10°	0°	0.52	9.2°	1.50

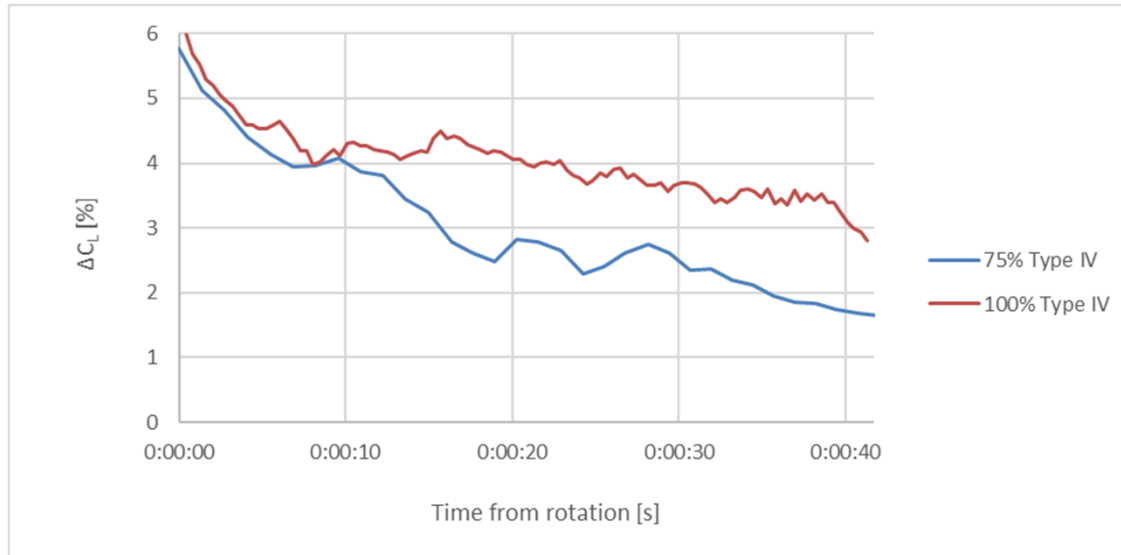
*$V_2 = 60 \text{ m/s}$ , rotation  $3^\circ/\text{s}$*

*Aerodynamic forces measured*

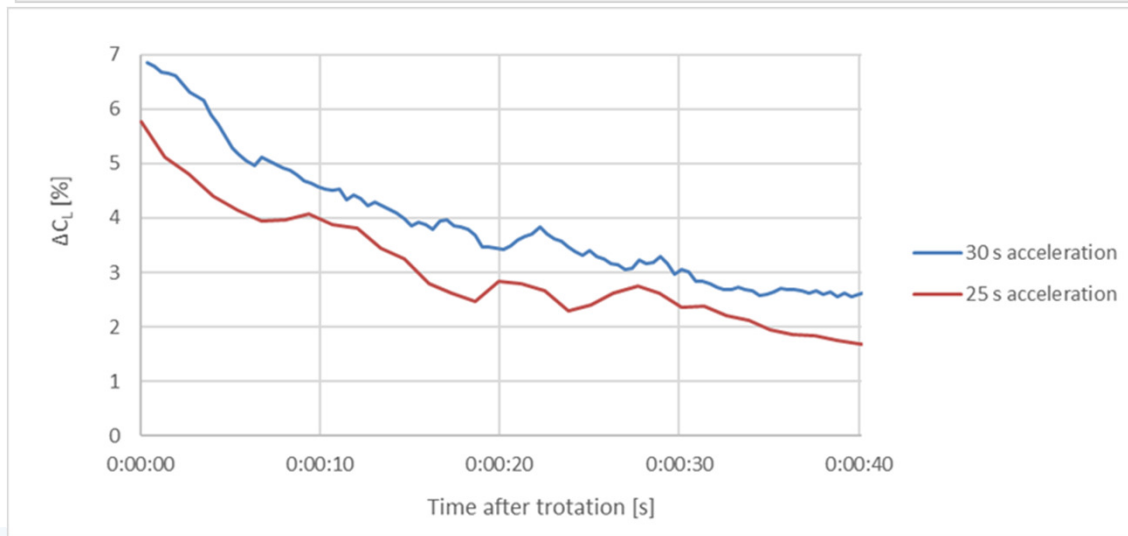
*B/L rake only for CRM*

*Fluid/Frost behavior video taped*

# Fluid Test Results – $\Delta C_L$ [%] in time

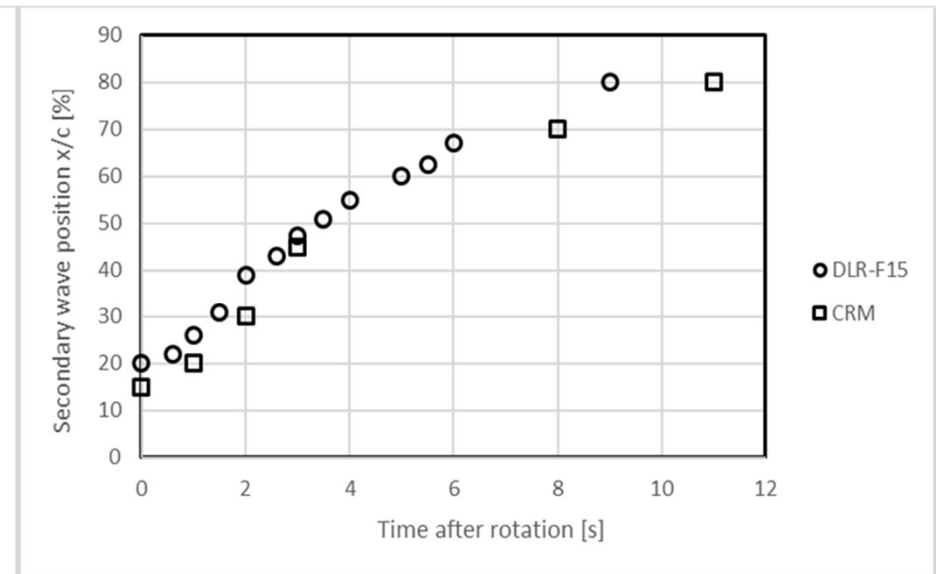
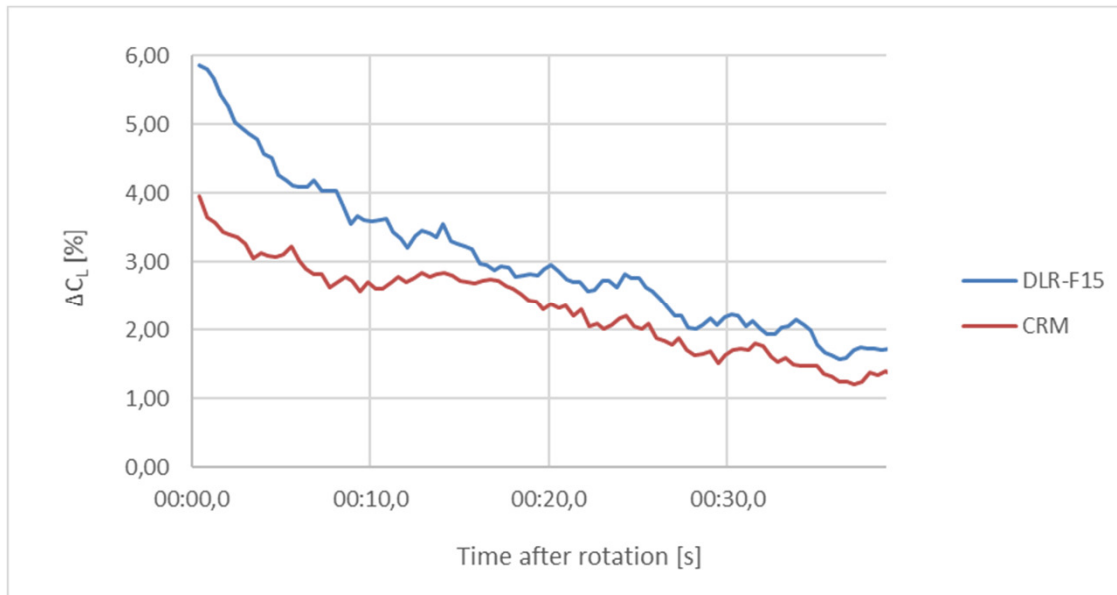


*Lift degradation from uncontaminated wing section in time after rotation DLR-F15, ambient  $T = -3^\circ\text{C}$  Diluted TIV  $\Delta C_L$  "hangs" quite high after rotation 30-40 s*



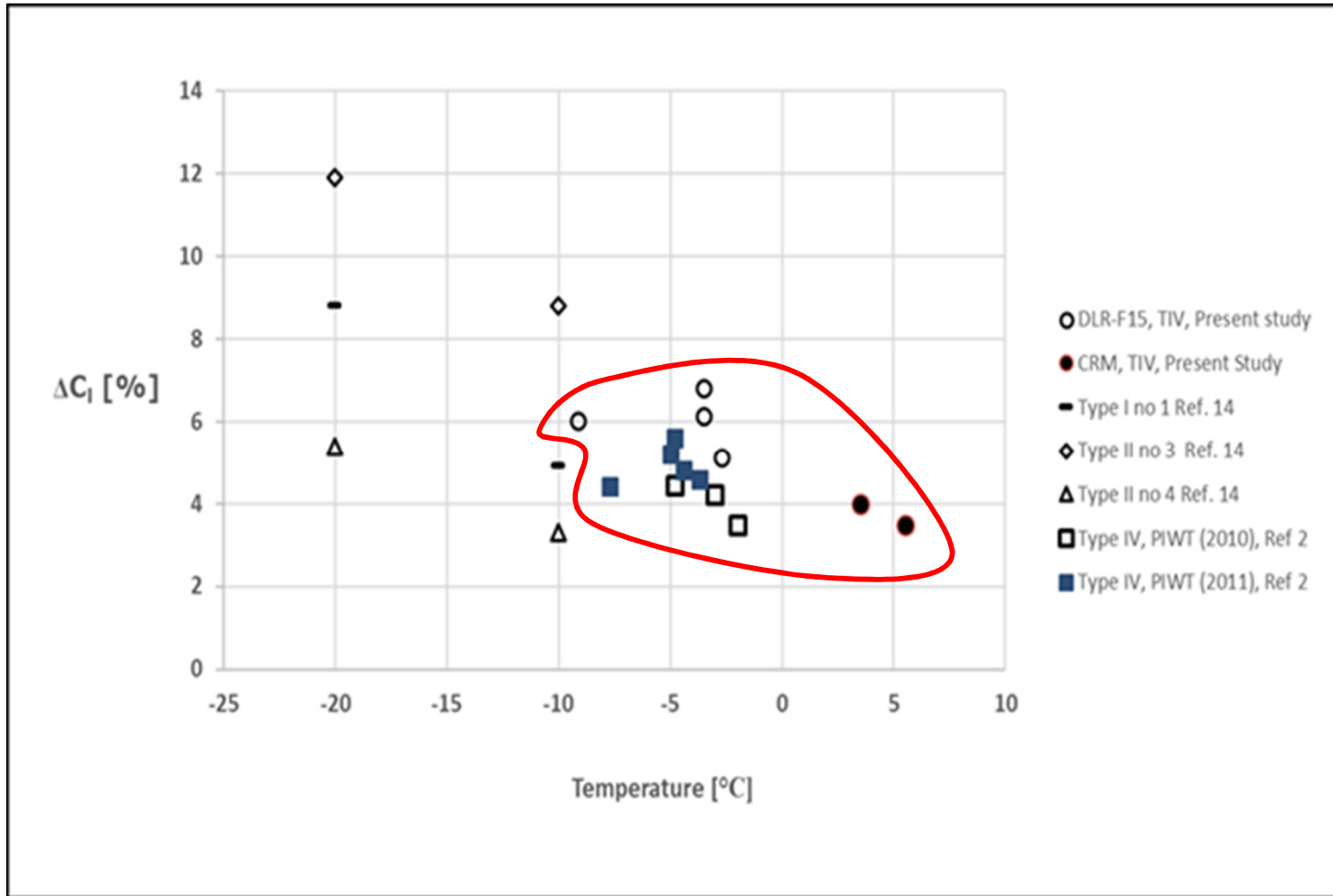
*Acceleration time has a simple time shifting effect on fluid induced lift degradation DLR – F15*

# Fluid Test Results – $\Delta C_L$ [%]



*The differences between the 2 wing sections tested are most probably due to different secondary waves. Further evidence by tests where the secondary wave effects were isolated (restricted fluid application, closed and sealed slat). Further tests indicated secondary wave contribution in the lift loss to be dominant*

# Fluid Test Results – $\Delta C_L$ [%]



$\Delta C_L$  immediately after rotation

Several studies

Cases isolated by red line: equivalent TIV fluid

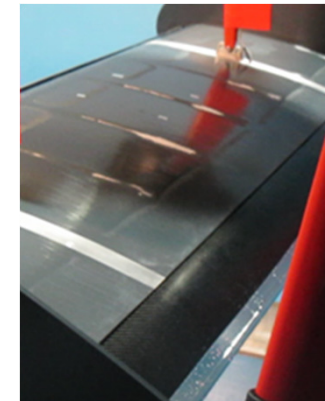
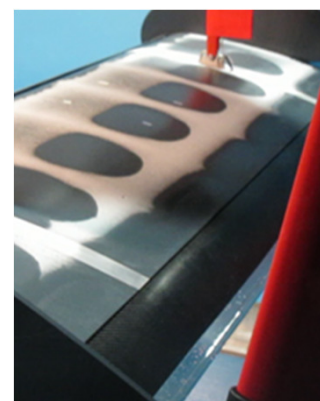
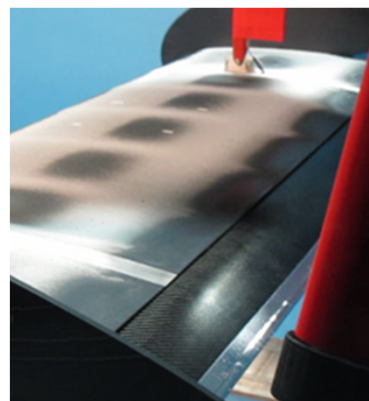
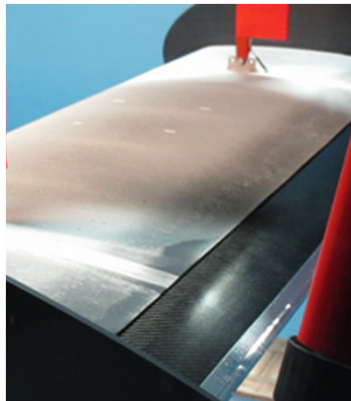
# CSFF W/T Test Results

*W/T speed and AoA sequence and measurements identical to fluid tests*

*17 different frost cases - thickness variation:*

$$k/c = 0.14 * 10^{-3} \text{ to } 3.60 * 10^{-3}$$

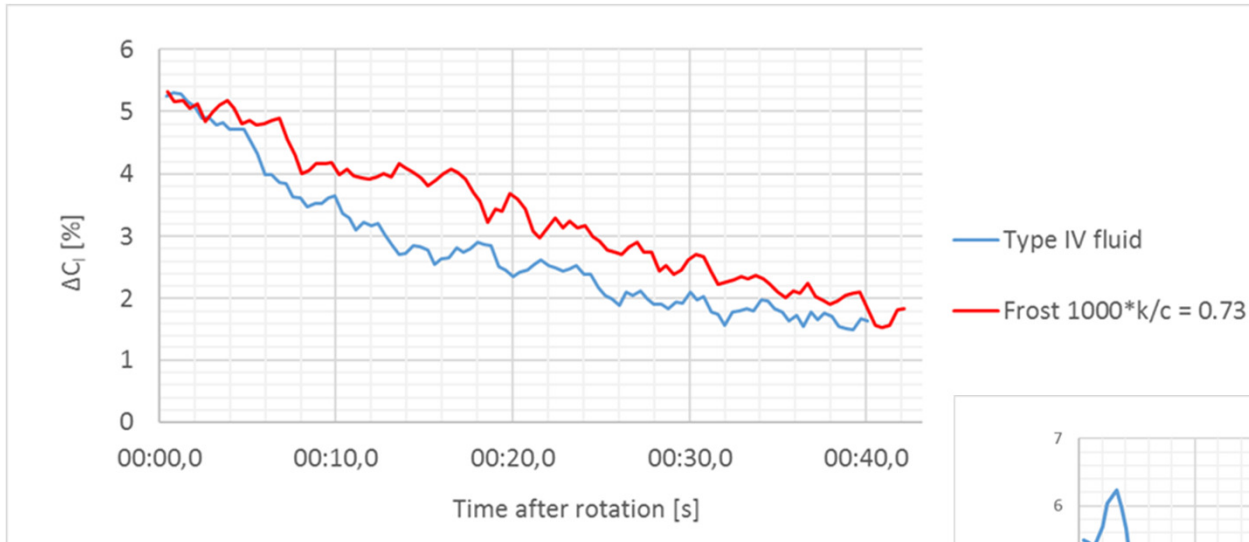
*Real frost – not sandpaper roughness → transient effects*



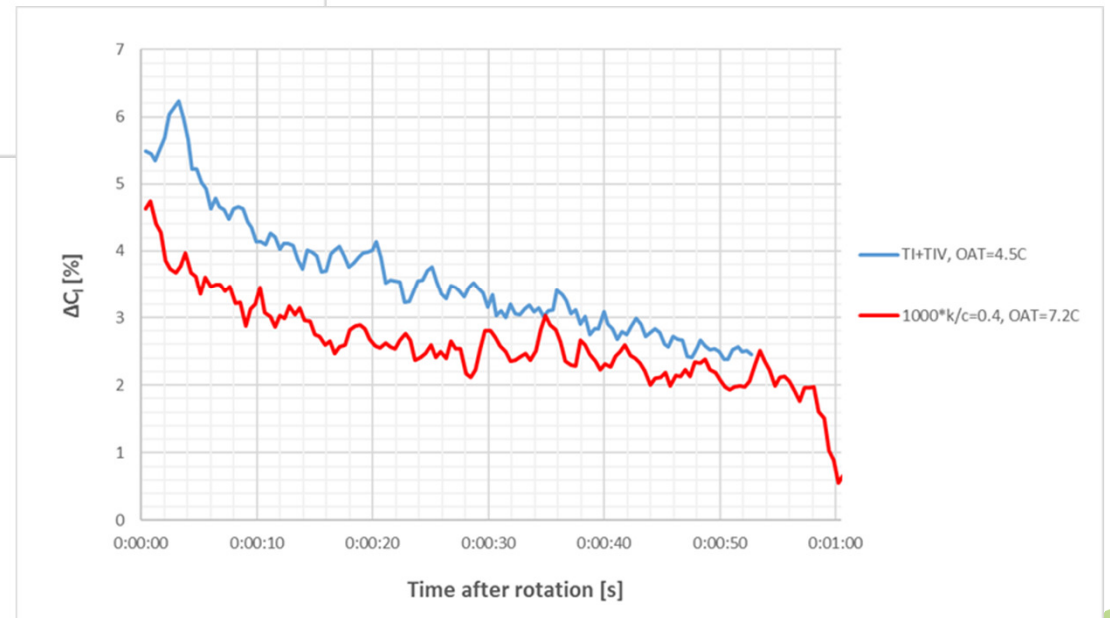
AoA=0° / U=38 m/s    AoA=0° / U=57 m/s    AoA=9.2° / U=60 m/s    30 s after rotation  
Ambient T = 7.2 °C and initial frost thickness  $k/c = 0.41 * 10^{-3}$



# CSFF vs. Fluids: Lift Loss Transiency

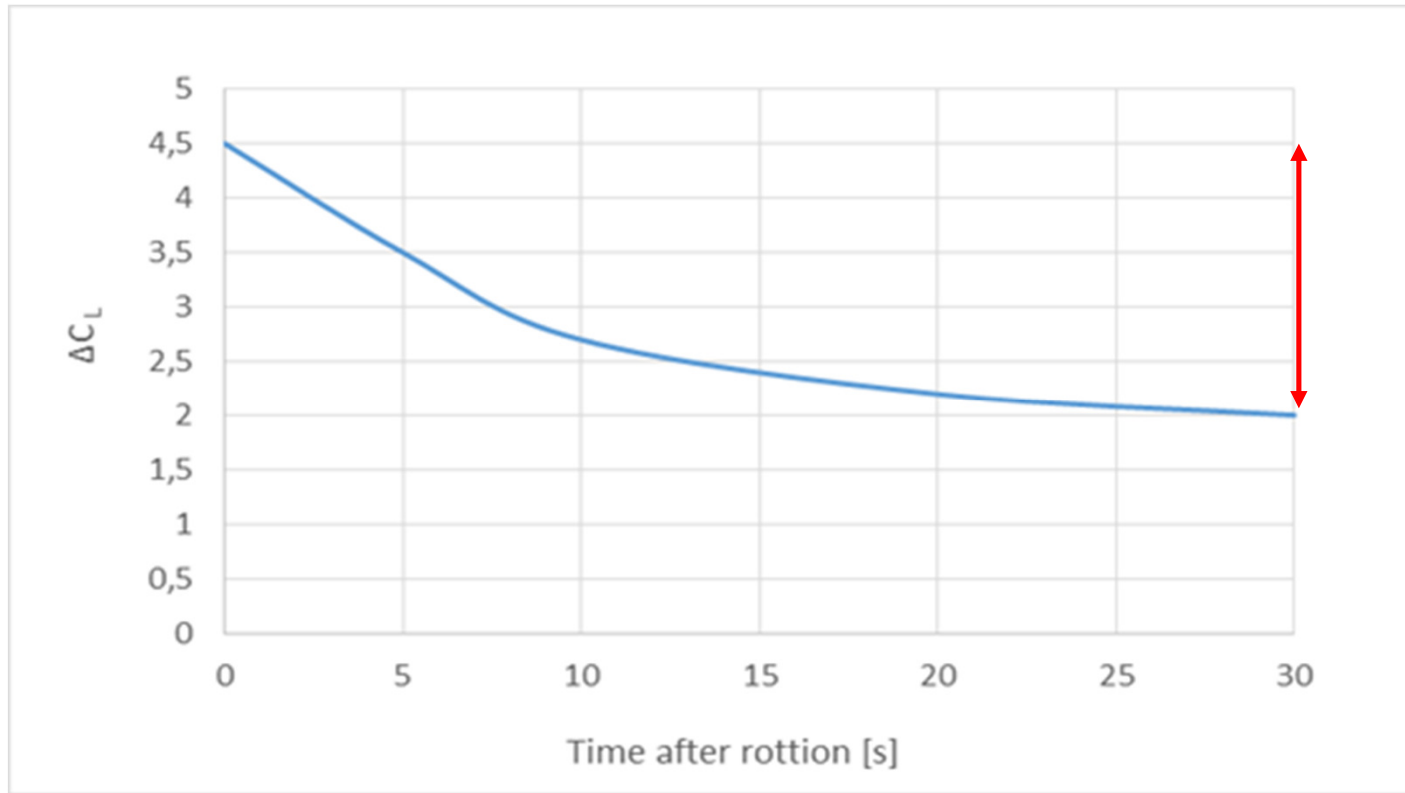


**DLR-F15**



**CRM**

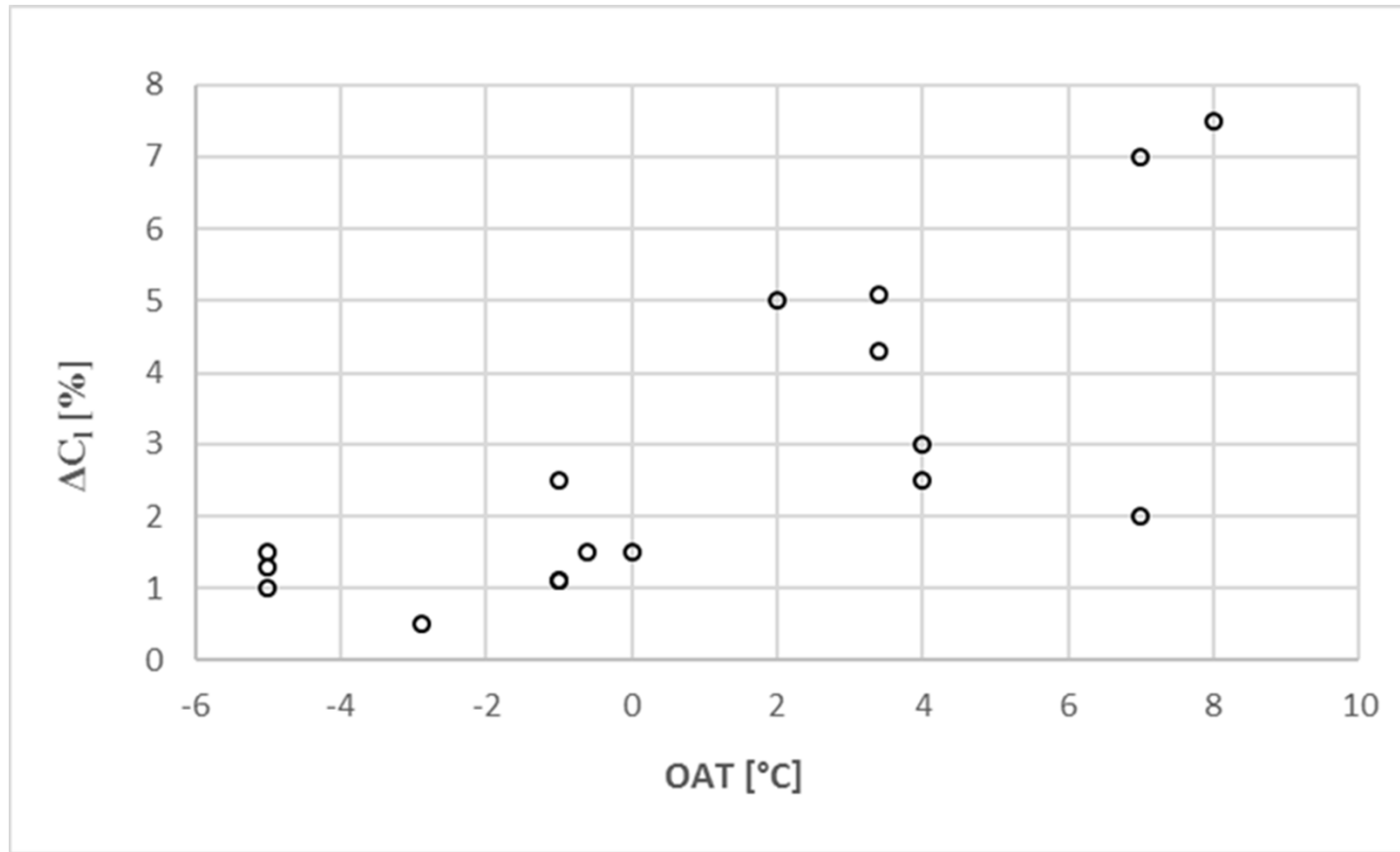
# CSFF Lift Loss Recovery



*Lift recovery in 30 s*

*Lift degradation [%] in time after rotation*

# CSFF Lift Loss Recovery



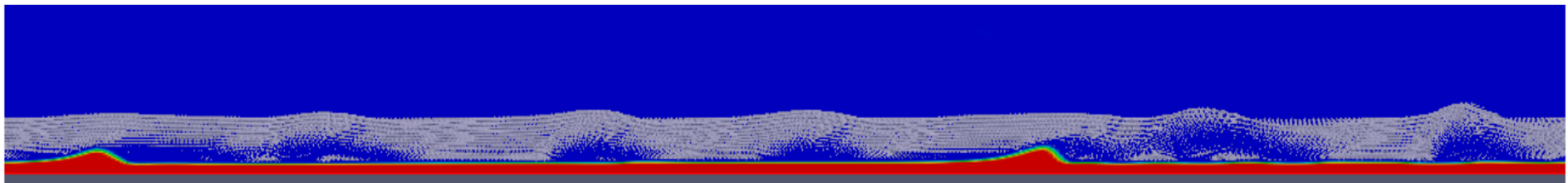
*Lift loss recovery (30 s after rotation) variation with ambient temperature*  
*Note: scatter at higher temperatures are due to effects during take-off roll phase*

The variation of lift coefficient recovery with air temperature after the first 30 s from rotation for a Cold Soaked Fuel Frost

- *Objective: study the possibility to estimate the fluid loss in time computationally without experiments*
- *A flat plate with a fluid layer in an accelerating airstream*
- *If the preliminary studies were successful there will be a theoretical method available to study the effects of fluid properties (density, viscosity and surface tension) on the fluid loss rate and FPET B-L displacement thickness*

- *Due to limited time/resources a 2D flat plate model was chosen*
- *Code applied: OpenFoam*
- *2 solvers available for 2-phase flow in OpenFoam code:*
  - *multiphaseEulerFoam*
  - *multiphaseInterFoam supports Non-Newtonian viscosity models, better stability, allows either LES or RANS turbulence models → this solver was selected*
- *2D grid for 0.6m long flat plate: 165 000 cells - recent trials with 1.8m flat plate with 480 000 cells*
- *Initial time step for 2D simulations  $5 \cdot 10^{-6}$  s → 5 second simulation for a 0.6m flat plate takes 2 weeks with 2 CPUs.*

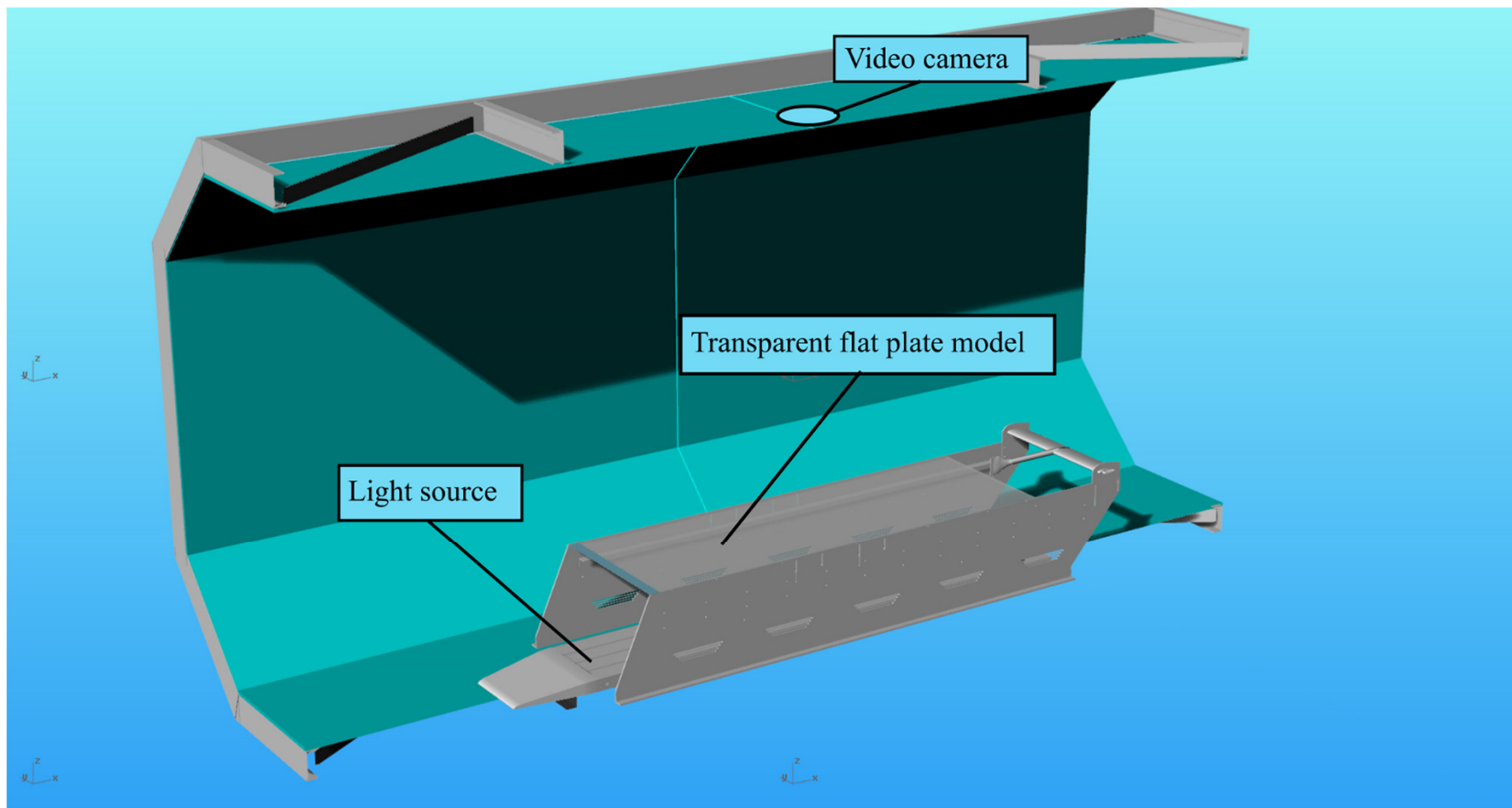
*Type I fluid (100 %) in airstream of 17 m/s – note airstream eddies*



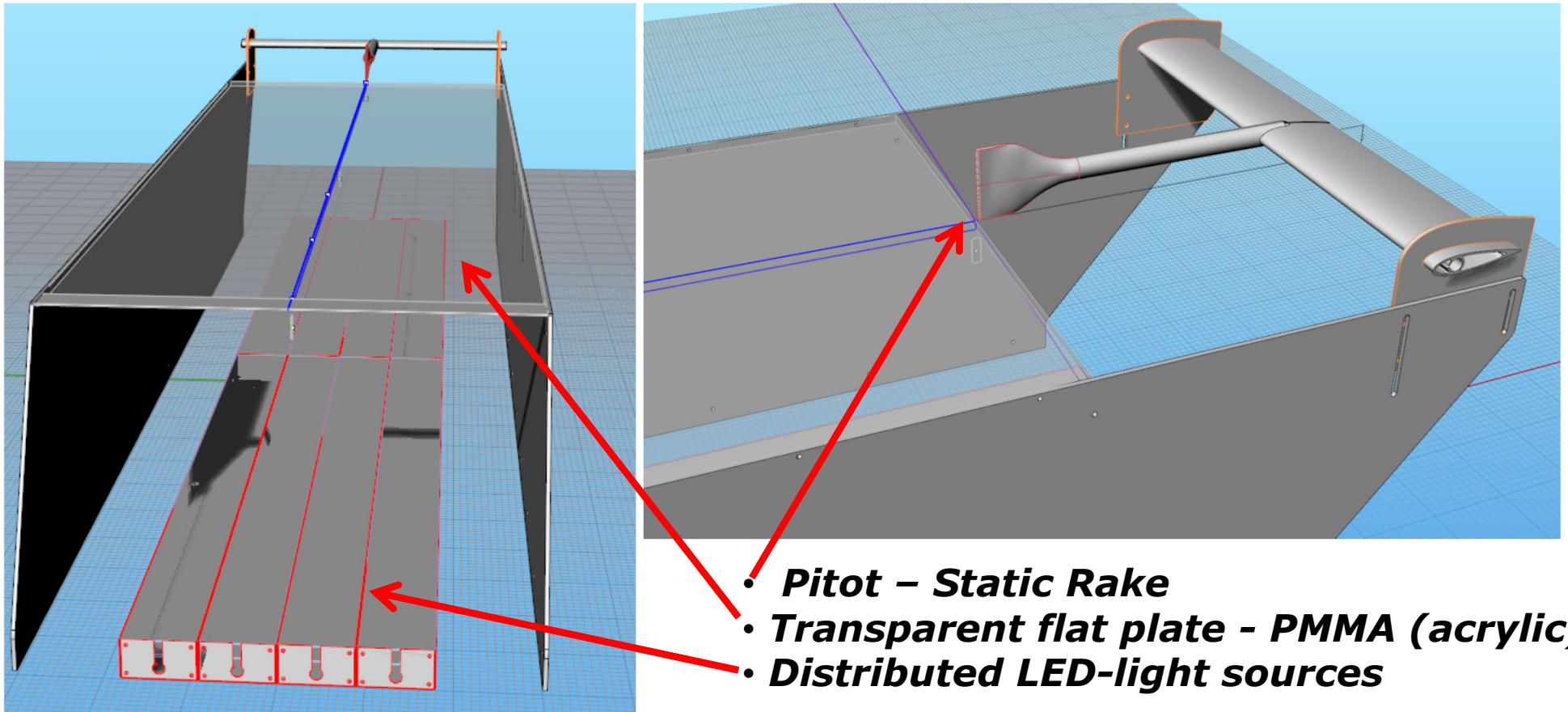
*To catch the effects of these eddies LES – turbulence model was chosen though it is considered essentially a 3D turbulence model*

*Selection was motivated by a fairly good 2 dimensionality of the waves according to W/T tests*

# Flat Plate W/T Tests to Evaluate CFD Calculations



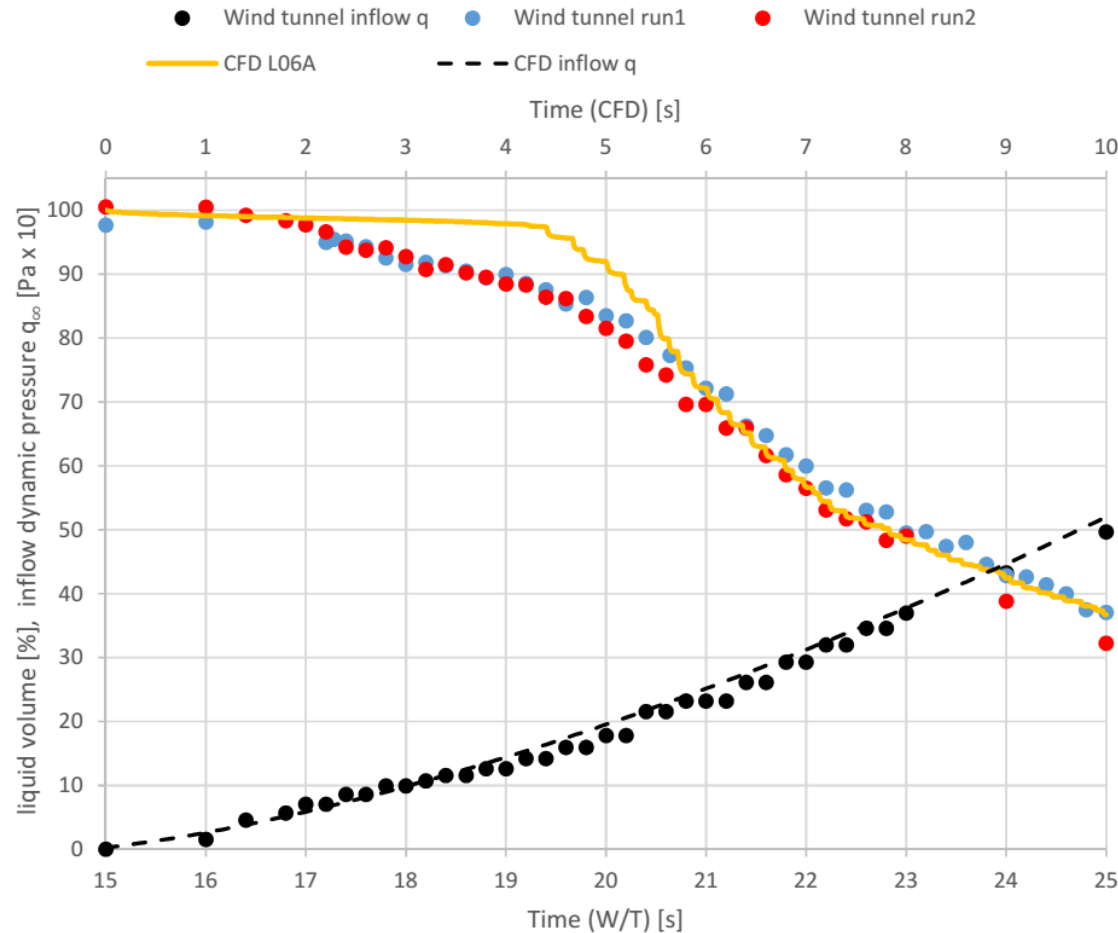
# Flat Plate Wind Tunnel Model



- **Pitot – Static Rake**
- **Transparent flat plate - PMMA (acrylic)**
- **Distributed LED-light sources**



# CFD Results Compared to Measurements



*0.6 m Flat plate*

*Total fluid volume variation and W/T kinetic pressure variation in time*

# CFD Studies - Continuation

- *Preliminary studies for Non-Newtonian fluids (TIV) have appeared challenging – at least for OpenFoam code. Needs more basic research*
- *Now in process TI fluids on a 1.8m flat plate and calculations for fluids at lower temperatures (-6 to -10° C) and higher viscosities (35 mPas to 170 mPas)*